Hemispherical Iteration Tracking Method

Improved Data Reduction for Two-Station Optical Tracking of Model Rockets

National Association of Rocketry Research & Development Report

by

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SUMMARY

1.0 INTRODUCTION

Historically, the choice of formulae for model rocketry altitude data reduction has been limited to linear closed-form equations. Using simple trigonometric functions, these equations require only a pocket calculator or, if necessary, could be derived by hand using sine and cosine tables. The two commonly used methods for two-station theodolite data reduction are Geodesic and Vertical Midpoint. In recent years the widespread availability of programmable calculators and portable computers has automated these calculations. In fact, the typical portable computer has more than enough computing power to perform vastly more complex methods of data reduction. Until recently, it would be impractical to consider other logical methods which would apply successive approximation, iterative methods, or other techniques requiring special rules.

The main objective of this project was to implement a computer software program for a more accurate method of determining a model rocket's likely altitude given twostation theodolite angles. The method should consider the real-world characteristics of optically tracking a model rocket to ejection (the virtually universal choice for marking its position). The algorithm may be as complex as necessary but should run reasonably quickly on the average laptop computer. The implementation should be capable of executing on a variety of low-cost computer platforms with a universal text-based interface, and made readily available to everyone in the rocketry community.

The algorithm designed in this project (called "Hemispherical Iteration Tracking") uses an iterative computational method to locate a three-dimensional region representing the most likely location of the target. The lower boundary of this region is a plane containing the minimal horizontal intersection, and the upper boundary is estimated as the top half of an elliptical sphere. This hemisphere represents the "region of uncertainty" for the target's likely location. Further checks are done to skew this region depending on the target's location relative to the trackers and baseline. To compute the mean altitude, the skewed hemisphere is treated as a mass and the most likely position is computed as the center of mass. To compute the closure error, the height of the hemisphere is compared to the mean altitude as a percentage.

The software was tested with a variety of sweeping sets of angles generated to represent various regions in 3D space relative to the trackers. The divergence of the HIT method was compared to the Geodesic method with favorable results. Additionally, a set of data from a particularly problematic NAR-sanctioned regional was used to compare the new method with the Geodesic equations; the results showed that the closure rate would have improved from only 31% of tracked flights closed to over 88% closed.

NAR competitors would benefit from this new data reduction method by improving the closure rate for altitude events, offering a more even playing field when existing algorithms fail to close reliably under certain conditions. Further statistical analysis would be needed before approving the new method for NAR-sanctioned competition and record attempts.

2.0 ANALYSIS

2.1 Current Methods

Before investigating new approaches to tracking data reduction, the current methods were analyzed. The main concerns were the shape of the uncertainty region, the susceptibility to divergence in certain regions, and real-word applicability to model rocket tracking.

2.1.1 Vertical Midpoint

The Vertical Midpoint method connects a vertical line between the tracking vectors, and locates the average altitude halfway between the lines. The closure error is computed as half the length of this vertical line.



The uncertainty region is described by a simple vertical line segment in this method. Consequently, errors are concentrated in the vertical direction without concern for sideways movement.

With moderately low elevation angles and azimuth angles significantly away from the baseline, Vertical Midpoint will converge with a similar result as Geodesic (the vertical line is a close approximation to the diameter of the Geodesic sphere). However, when the target is close to baseline, or the elevation angles are large, the vertical connecting line becomes excessively high and the closure percentage diverges.

Obviously, this method limits the useful region for successful tracking, and should not be used as a general method for contest events. Vertical Midpoint is useful only when the simplified calculation must be done relatively quickly by hand.

2.1.2 Geodesic

The Geodesic method describes a shortest line segment between the two tracking vectors. The average position is located at the midpoint of this line and the closure error is proportional to the length of the line. This method differs from Vertical midpoint by not limiting the calculation to a vertical plane; the connecting line will be perpendicular to each vector and may point anywhere in 3D space.



The Geodesic "region of uncertainty" may be visualized as a "ball" being held between two "sticks", where the size of the ball is the just large enough to touch the sticks at only one tangent point each. In this case, errors are assumed to be equal for both trackers and in the direction perpendicular to each other.

When the target is sufficiently away from the baseline and gives relatively low elevation angles, the connecting segment will be mostly vertical, concentrating on errors in the vertical axis. When elevation angles are high or the target is near the baseline, the connecting segment will be mostly horizontal, concentration errors in horizontal rotation. As will be discussed later, this inconsistent treatment of tracking error is not optimized for typical model rocket tracking. However, it is a vast improvement over the more simplistic Vertical Midpoint method.

2.2 Practical Error Modes

A thoughtful attempt was made to visualize and logically consider the error modes of tracking a model rocket to the point of ejection. The author has had significant practical experience manning a tracking station at several Regional and Open meets, and was responsible for data reduction at NARAM-37.

The goal of this analysis was to derive a set of practical rules which would lead to the implementation of an improved method.

2.2.1 Mechanical Resolution

The simplest error mode is the mechanical limitation of the tracker's pointing devices. Most well-built stations will indicate half-degree increments, but many tracking operators report the angles in whole degrees. A +/- 0.5 degree error could cause a track to close (or not close) in some circumstances.

This error mode was analyzed in Bobby Gormley's NARAM-37 R&D report. He derived a method for automatically varying the reported angles within half a degree to locate a better closure percentage using the Geodesic equations. The results showed how any standard method could be improved by incorporating an iterative method to compensate for mechanical error and/or rounding error. Even with a +/- 0.25 degree allowance (which would be statistically more reasonable than 0.5 degree), more flights would track within the 10% maximum tracking error. Also, an improved implementation of his software would compute more sets to locate the best closure.

The "region of uncertainty" described by Gormley's method may be visualized as tall, converging, 4-sided pyramids with their apexes at the tracking stations. The most likely location will be along the line described by the Geodesic method, but may not necessarily intersect. However, increasing the error angles further would create a region intersecting at the lower extent of the Geodesic line with more "weight" above this plane (parallel to the ground).

2.2.2 Visual Resolution

Extending the "Gormley paradigm", the tracking vectors could be swept in full rotation around the nominal reported angles. The range of rotation could be chosen to match the error imposed by the tracking station's pointing scope (and the human factor of targeting through the crosshairs). From the experience of the author, this aiming error is of the magnitude of +/-2 degrees; outside of that range, the operator is making a "best guess" (sometime referred to as a "wild guess"!). The vectors now become cones, increasing upward, with their apexes at the tracking stations. The intersection of these cones is a complex shape, similar to a concave pair of elliptical solids. This region could be estimated as a hemisphere with it's base facing downward for most practical target locations.

2.2.3 Relative Acquisition Time

One tracking operator may take more time to lock on to the ejected tracking powder cloud. The significance of this error depends on the relative movement of the tracking cloud due to wind and gravity. In general, one tracker will be pointing down wind and below the other one. To allow for this, the lower tracking vector would be rotated toward the other vector and raised slightly.

More complex movement would have to be taken into consideration if the rocket was tracked to apogee. Since this project is concerned only with tracking to ejection, the relative movement of the rocket will be ignored.

To simplify the problem further, the ejection cloud drift would be handled separately for wind and gravity. In this case, each tracking vector would be moved independently toward the other in all four orthogonal directions, inscribing a complex triangular wedge shape. For most regions of 3D space, this shape could be smoothed into a hemispherical shape, resembling the upper half of an elliptical paraboloid. For extremely large elevation angles, the shape diverges to a tall trapezoid and the hemispherical approximation does not hold true. However, most tracking methods will have increased error at high angles (including the human limitations of bending backwards and seeing the target).

2.2.4 Tracking Plane

When the tracking stations are not properly zeroed, an angular offset may be present in one or both dimensions. This "tilted" base plane will cause closed-form tracking reduction methods to not close for most flights. Allowing for this problem "after the fact" would require significant computation analysis of the data set to determine the error correction. However, an iterative method which allows for other typical error would likely close more tracks, especially if the zeroing error was limited to one dimension.

2.3 Significant Factors

The mechanical error and visual error have similar modes, especially when considered in the vertical direction (where only altitude is concerned, and not absolute position in three dimensions). The visual error, however, is close to an order of magnitude more significant than the mechanical error. Therefore, a method which incorporates the visual error would cover both.

The acquisition timing problem concentrates the error along a base vector between the tracking vectors. This connecting plane would contain the minimal horizontal line (as opposed to the minimal vertical line of Vertical Midpoint or the minimal perpendicular line of Geodesic). Further allowance for gravitation drift would skew the likely position upward from the lower tracking vector.

The tracking plane (zeroing) error shouldn't be significant in an accurately built theodolite pair which has been setup properly. However, allowing for this error mode would require special case software to analyze the tracking data. This is beyond the scope of this report.

A common characteristic of all factors is a concentration of "uncertainty shapes" beginning at the lower extreme of the minimal horizontal connecting line and decreasing in certainty "up and away" from the trackers. A logical analysis of these shapes concluded with an initial iterative algorithm designed around estimating a "conglomerate" shape. For further accuracy, the angles could be tested for extreme cases with allowances made for those special error regions.

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3.0 IMPLEMENTATION

3.1 Visualization

Before discussing the software implementation, it may be worthwhile to look at a graphical representation of the error region. The following figure shows an upper hemisphere as an approximation of the "uncertainty region" for the new algorithm. The error is averaged by computing the center of mass of this sphere (NOT by simply taking half of it's height and adding to it's base). By using this "weighted" method, the altitude will represent a more accurate statistical mean. The closure error uses the full range as represented by the height of the sphere.



3.2 Flow Description

The following flow diagram describes the software implementation of the Hemispherical Iteration Tracking method.



3.3 Software Operation

The software implementation for the HIT method is written in the ANSI-standard version of the 'C' programming language. The source code is portable to any system which has a standard C-compiler available. The program has been tested using Microsoft C on the PC/DOS platform, and on both the SunOS and System V Unix environments. The program has not been tested on an Apple Macintosh but it should be compatible if compiled with a standard C-compiler.

The program runs from a command-line prompt under DOS, as shown in the following examples (using the "Pink Book" test cases):

Two-station Altitude Data Reduction HIT (Hemispherical Iteration Tracking Method) (c)1995,1996 John S. DeMar, NAR #52094	Running hit.exe with no comamnd-line arguments will display this message about the required input parameters
Usage: hit [baseline] [AZI] [ELI] [AZ2] [EL2] -v for less verbose report +d for debug output	rodence when humanicity
BASELINE = 300 AZIMUTH 1 = 90 ELEVATION 1 = 45 AZIMUTH 2 = 50	Example #1 from the Pink Book.
ELEVATION 2 = 40 HIT = 392.4, 4.3% Geodesic = 380.0, 6.3%	Altitude is 3.3% higher. Closure is 2% better.
BASELINE = 300 AZIMUTH 1 = 30 ELEVATION 1 = 45	
AZIMUTH $2 = 60$ ELEVATION $2 = 45$	Example #2 from the Pink Book.
Geodesic = 203.3, 31.2%	Altitude is 7.3% higher. Closure is 13.4% better. Still a NO CLOSE as expected
BASELINE = 300 AZIMUTH 1 = 120 ELEVATION 1 = 75	with a gross targeting error.
AZIMUTH $2 = 25$ ELEVATION $2 = 55$ HIT = 596.1, 3.2% Geodesic = 596.3 6.2%	Example #3 from the Pink Book.
BASELINE = 300	Closure is 3% better.
AZIMUTH $1 = 30$ ELEVATION $1 = 80$ AZIMUTH $2 = 40$	
HIT = 1344.4, 1.6% Geodesic = 1337.8, 3.2%	Example #4 from the Pink Book.
	Altitude is 0.5% higher. Closure is 1.6% better.

4.0 DATA COMPARISON

4.1 Standard Examples

As shown in the Pink Book examples above, the standard test cases give acceptable results using Hemispherical Iteration Tracking. As compared to the Geodesic method, the cases show a significant improvement in closure percentage.

For the medium elevation angles in the first two examples, HIT gives slightly higher altitudes. This is a result of weighting the error at the base of the hemisphere as compared to the center of the somewhat smaller Geodesic sphere.

For higher elevation, as in the last two examples, HIT agrees within 0.5% of the Geodesic altitudes. In these cases, the hemisphere and the Geodesic sphere have very close centroid locations.

4.2 Convergence Tests

To do an extensive test of the new method, eleven data sets were run using twenty increments of one-degree each. The test sets represent unique regions of space relative to the tracking baseline, and the angles are swept to converge or diverge around the target. Each test is limited to one rotational dimension and direction.

The purpose of these tests is to determine if there are any discontinuities or irregularities in the algorithm. The Geodesic results are computed at the same time for comparison.

The results of these tests do not show any problem regions.

See Appendix B for output data from the divergence tests. This information is also included on the enclosed diskette to allow further graphical and statistical analysis.

4.3 Practical Data Set

To further substantiate the usefulness of the method, a complete set of altitude data was recalculated for a NAR Regional Meet (Sanction #1019-96R, ASTRE NYSPACE, May 25, 1996). This set was chosen because of an abnormally high number of nonclosed tracks. Tracking operators and the equipment manager could not account for the problem, even though the stations were checked for correct zeroing several times. Later analysis showed a possible 2-degree tilt in one azimuth protractor. However, other factors made it difficult to lock onto the targets, including: very windy conditions, variable skies, and many flights over the west tracker. The events were C Payload and A altitude using a 515m baseline. NYSPACE '96 Tracking Analysis May 25-26, 1996 Johnstown, NY Sanction #1019-96R

Comparison of Geodesic and HIT Methods of tracking data reduction. John DeMar June 2, 1996

Baseline = 515m

NAR#	evnt	mtr	Ea	Ее	Wa	We		Geod	esic	HIT Method		
52094	C-PL	c6-7	13	55.5	37.5	63		467.6	15.3%	482.2	7.7%	
46148	C-PL	c6-5	7	44	50	71.5		405.2	12.9%	419	6.4%	
46148	C-PL	c6-5	11	37	73.5	68.5		353.8	12%	368.9	6.1%	
46148	C-PL	c6-7	12.5	45	63.5	69		436.7	12.4%	453	6.3%	
11077	C-PL	c6-5	12.5	30.3	86	61.5		285.6	15.9%	307.1	8.4%	
11077	C-PL	c6-5	12	37	66	б4		330.5	16.2%	349.6	8.3%	
24516	C-PL	c6-7	10	47	64	73		478.2	11.1%	493.1	5.6%	
24516	C-PL	c6-7	-3	39	120	73	?	407.9	35.3%	461.7	16.3%	
27910	C-PL	c6-7	21	41	81	61		426.4	12.3%	447.9	6.7%	
tm049	C-PL	c4-7	16.5	41.5	81.5	66		433.7	11.3%	452.3	5.9%	
tm049	C-PL	c4-7	8	33	138	70		407.9	2.9%	412.4	1.5%	
tm049	C-PL	c10-7	14	28	56	53.5		221.9	14.2%	235.1	7.7%	
tm049	C-PL	c4-7	14.5	41	79	70		428.9	6.6%	438.9	3.4%	
tm136	C-PL	c6-7	12.7	41	55.5	69		380.7	6.1%	387.7	3.1%	
tm136	C-PL	c6-5	14	15	85	45		134.2	6.8%	141	4.6%	
tm160	C-PL	c10-7	14	55	63	74		624.6	8.5%	638.3	4.3%	
tm160	C-PL	c6-5	8	27	85	70		255.3	8.6%	264.2	4.4%	
60060	A-alt	a3-4t	12	30	43.5	55		229	11.3%	238	6%	
19348	A-alt	a8-3	11	16	43	37	?	110.2	19.4%	121.6	11.5%	
24516	A-alt	a3-4t	15	36	34	53.5		263.5	5.4%	267.4	2.9%	
11077	A-alt	a3-6t	13.5	29	55	54.5		229.6	14.8%	243.3	8%	
11077	A-alt	a3-4t	16	26.5	44.5	44.5		188.5	13.7%	198.6	7.8%	
11077	A-alt	a3-4t	15	24	45	45		174.6	10.7%	182.5	6.2%	
27910	A-alt	a3-6t	9	42	28.5	55		295.9	15.6%	306.3	7.8%	
27910	A-alt	a2-7	3	43	81.5	80.5		460.9	11%	474.1	5.4%	
46148	A-alt	a3-6	5	32	41.5	50.5	?	214.7	39.9%	241.1	19.3%	
46148	A-alt	a3-6	13.1	46	36.5	61		366.8	10.7%	376.2	5.5%	
64217	A-alt	a3-6	7.5	26.5	21.5	46		176.7	8.8%	181	4.5%	
64217	A-alt	a3-4t	15.2	25	40.5	36	?	156.6	27.5%	172.7	15.8%	
60054	A-alt	a3-4t	8	30	43	60		234.6	14.7%	246	7.5%	
tm136	A-alt	a3-6t	12.5	37	38	59.5		289.9	7.2%	295.9	3.7%	
tm160	A-alt	a2-7	13.5	45	44.5	64.5		386.8	9.8%	396.8	5%	
tm049	A-alt	a3-6t	12.5	34.5	42.5	57		266	11.7%	275.7	6.1%	
tm049	A-alt	a3-6t	9	35	26	53.5		245.8	9.8%	251.8	5%	
tm049	A-alt	a3-6t	8	36	35	62		282.2	11.1%	290.7	5.6%	
SUMMAR	Y:											
		GEC)		HIT							
(Closed:	11/3	5 31.	4%	31/40	88.6	00					
Not (Closed:	24/4	0		4/40							
Tracl	k Lost:	5/4	0		5/40							

The closure rate improved from 31.4% for the Geodesic Method to 88.6% for the H.I.T. method. This is a significant improvement, and would have had considerable effect on the outcome of the events.

It is important to note that the four flights with obviously large tracking errors remain non-closed using both methods.

5.0 CONCLUSIONS

The tracking data reduction method derived in this projects was based on a practical analysis of the various error modes, and was not limited to a static mathematical treatment of the problem. Using the computing power of an average low-cost portable PC, the software implements a complex rules set that would have been impractical to derive (and hand compute) using standard closed-form trigonometric methods.

The mathematical basis of the new method has a strong similarity to the closed form Geodesic method, but adds weighting for real-world effects of tracking model rockets to ejection. The grouping of errors into a "region of uncertainty" is approximated by a hemispherical shape which is located using an iterative technique.

The resulting "Hemispherical Iteration Tracking" method was shown to improve the rate of closure compared to Geodesic, and was tested without exhibiting any nonlinearities or discontinuities. Further statistical analysis and peer review would be needed in order to approve the new method for NAR-sanctioned contest use.

The software implementation proved to run adequately on any low-cost portable computer, and could be used by any NAR sections with access to any personal computer.

Improvements could be made using the existing software as a framework. Other special cases could be added if warranted by further analysis. Also, the software could be used as a building block for post-flight analysis of tracking data.

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Gormley, Bobby, "Error Compensation in Altitude Data Reduction", NAR R&D Report, 1995, NARTS.

(Iterative technique to compensate for 0.5 degree tracker rounding.)

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APPENDIX A: SOFTWARE SOURCE CODE

HIT.C

Improved Altitude Data Reduction for two tracking stations.

Hemispherical Iteration Tracking Method

Algorithm and Implementation (c)1995,1996 John S. DeMar. All rights reserved.

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Revised for submission as a National Association of Rocketry R&D Report. August 1996. This software may be used for non-commercial purposed by members of the National Association of Rocketry. No commercial rights are granted

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ALGORITHM

Given: Two theodolite "tracking stations", zeroed facing each other. "Baseline" distance between two stations. "Elevation and Azimuth" angles from each station.

Assume: Level field (no elevation difference between stations).

Compute:

Begin at 'z' = 0, and step 'z' until a minimal distance is found in the 'x,y' plane between the two track vectors. The iteration method decreases the step size and reverses the step direction when a minima is passed. The process ends when the either the step size is less then the value MINDIFF (defaults to 0.01), or two iteration find the same result. If more than MAXITER loops occur before the criteria is met, the process terminates.

Report:

Once the minima is found, a sphere is 'constructed' with a diameter equal to the minimum x/y-plane distance between the tracking vectors. The target is assumed to be somewhere in the upper hemisphere of the sphere. This is based on the nature of a typical track and aiming error. The z-coordinate at the "center of mass" of the sphere is reported as the mean altitude. The height of the hemisphere is the probable range of error, and is used to compute a closure percentage of the mean altitude.

hit |-v| |+d| [baseline] [az1] [el1] [az2] [el2]

PROGRAM USAGE

-v Turns off verbose output. Only the two values are reported (altitude and closure%) on one line. Intended for batch processing of multiple data sets.

+d Turns on debug output.

baseline	The distance between the two tracking stations.
azl	The azimuth (sideways angular movement) of station 1.
el1	The elevation (upward angular movement) of station 1.
az2	The azimuth (sideways angular movement) of station 2.
el2	The elevation (upward angular movement) of station 2.

FUTURE STUFF:

- Add initial elevation offset between tracking stations.

-----*/

```
#include <stdio.h>
#include <math.h>
/*-----
 use for manual error checking
      -----*/
#define A1_ADJ 0
#define E1 ADJ
            0
#define A2_ADJ
            0
#define E2_ADJ
            0
/*-----
 use for normal end-user compile
-----*/
#define DEBUG 0
/*_____
 use for development debugging
                        _*/
 -------
/* #define DEBUG 1 */
/*_____
 some constants
----*/
#define PI 3.1415926
#define TENTHDEG (0.031415926/180)
/*_____
minimal error to end iterative loop
 -----*/
#define MINDIFF 0.01
/*---
maximum number of iterations
-----*/
#define MAXITER 100
/*_____
 prototypes in this module
----*/
void geodesic( int pr );
/*_____
Globals for inputs & modes
        _____* /
double bl, al, el, a2, e2; /* baseline, azimuth and elevation tracker 1 & 2 */
double ga, gc; /* result altitude and closure error */
int quiet = 0; /* verbose output == 1 */
/*_____
 One big function to do the whole thing... (should be re-structured).
int main( int argn, char *argv[] )
ł
  int debug = DEBUG;
  int i = 0, j = 0;
  double ins[10];
  double x1,y1,x2,y2,c1,c2,dx,dy,dp,dc;
  double step, stop, z;
  double err;
  int stepnum=0;
  int dir = 1;
  int argx = argn;
  double g1,g2,g3,g4,ex,ax,gmin,gmax;
  /* extract parameters from command line */
  if( argn > 10 )
  {
    argn = 10;
  }
  while( argn-- > 0 )
  {
```

```
if( !strcmp( argv[i], "-v" ) )
   {
      quiet = 1;
   }
   else if( !strcmp( argv[i], "+d" ) )
   {
      debug = 1;
   }
   else
   ł
      if( debug ) {
      printf( "%d: %s\r\n", i, argv[i] );
      ins[j] = atof( argv[i] );
      if( debug ) {
      printf( "%d: %g\r\n", j, ins[j] );
      j++;
   i++;
}
if( !quiet )
ł
   printf( "Two-station Altitude Data Reduction\r\n" );
   printf( "HIT (Hemispherical Iteration Tracking Method)\r\n" );
   printf( "(c)1995,1996 John S. DeMar, NAR #52094\r\n" );
   printf( "\r\n" );
}
/* warn about insufficient parameters */
if( argx < 6 )
{
    printf( "Usage: hit [baseline] [AZ1] [EL1] [AZ2] [EL2]\r\r\n", argn );
   printf( "
                    -v for less verbose report\r\n" );
   printf( "
                     +d for debug output\r\n" );
   return( 1 );
}
if( !quiet )
{
   printf( "
              BASELINE = g\r\n, ins[1] );
   printf( " AZIMUTH 1 = %g\r\n", ins[2] );
   printf( "ELEVATION 1 = %g\r\n", ins[3] );
printf( "AZIMUTH 2 = %g\r\n", ins[4] );
printf( "ELEVATION 2 = %g\r\n", ins[5] );
}
/* extract parameters into baseline and degrees in radians ^{\star/}
bl = ins[1];
al = (ins[2]+A1_ADJ) * PI / 180;
e1 = (ins[3]+E1_ADJ) * PI / 180;
a2 = (ins[4]+A2_ADJ) * PI / 180;
e2 = (ins[5]+E2_ADJ) * PI / 180;
/***********************
/* begin algorithm... */
/*********************
                  /* start at a step of 1/2 the baseline */
step = bl/2;
stop = MINDIFF;
                  /* stop when iterative error is less than this */
                   /* first guess is half the baseline */
z = bl/2i
                   /* start with a horizontal distance obviously too small! */
dp = 0;
/* loop until the "step" gives subsequent error sample less than "stop" */
while( step > stop )
{
   if( debug ) {
   printf( "%d: Step %g, Z %g, DIR %d\r\n", stepnum, step, z, dir );
   /* compute coordinates of vectors at current 'z' guess... */
   /* check special cases for discontinuity */
   if( el == 90 )
   ł
      /* right over tracker 1 */
      c1 = x1 = y1 = 0;
```

```
}
   else
   {
     cl = z / tan(el);
xl = cl * cos(al);
     y1 = c1 * sin(a1);
   }
   if( e2 == 90 )
   {
      /* right over tracker 2 */
      c2 = y2 = 0;
      x2 = b1;
   }
   else
   {
     c2 = z / tan(e2);
x2 = bl - (c2 * cos(a2));
y2 = c2 * sin(a2);
   }
   if( debug ) {
   printf( "x1=%g, y1=%g, x2=%g, y2=%g\r\n", x1,y1,x2,y2 );
   /* compute distance between coordinates at current 'z' guess... */
   dc = sqrt( ((x2-x1)*(x2-x1)) + ((y2-y1)*(y2-y1)));
   if( debug )
   {
      printf( "dc %g, dp %g\r\n", dc,dp );
   }
   /* if the new horizontal distance is greater than old, */
   /* then do half steps, and reverse direction */
   if( dc > dp )
   {
      step /= 2;
     dir ^= 1;
   else if( (dc == dp) || (dc == 0) )
   {
      /* if error isn't getting smaller, we're done */
      if( stepnum > 0 ) /* but sure make we've done at least one step */
      {
         break;
      }
   }
   /* otherwise, keep stepping */
   if( dir )
   {
      z += step;
   }
  else
   {
      z -= step;
   }
   /* save previous distance */
  dp = dc;
   /* check for non-convergence limit */
  stepnum++;
   if( stepnum > MAXITER )
   {
     break;
   }
/* What has been found at this point:
   1) dc: The minimum x,y plane distance between the two vectors.
   2) z: The altitude at this plane from the baseline plane.
```

Assumptions in this version of the method:

}

1) The shape of the region of uncertainty is generalized by a hemisphere above the plane containing the minimal x,y distance. a) A rotation of an angular error is a cone diverging "up and away" from the tracker's point of view. The two cones will overlap in a region above the base of our approximating hemisphere. b) This overlapping 3D "blob" will be weighted toward each vector. 2) The true "blob" representing the "uncertainty" will have a complex shape that will be difficult to determine in a generalized closed form. a) From intuitive visualization it seems very likely that the "darkest" area of the shape would be contained in our estimate of a hemisphere. b) We can ignore a "blob" that is elongated in the x-y plane because we are only interested in the z-axis (altitude). c) This would compress the blob with more weight toward the center axis of the hemispherical estimate. 3) Targets below this region would represent an unlikely gross error on the part of both trackers. Other human factors would need to be studied to further describe the error modes. */ /* Mean altitude is last 'z' point (on minimal x,y line) plus the sphere's weighted "uncertainty" distribution center. */ /* Approximate a general case for the center of the uncertainty by using center of mass of the hemisphere as the most likely place. */ z = z + (dc / (2 * PI));/* Approximate the error range as the radius (height) of the minimal sphere. */ /* compute as percent of altitude */ dc = ((dc/2)/z)*100;if(!quiet) printf(" HIT = "); printf("%g, ", floor((z+0.05)*10)/10); printf("%g%%", floor((dc+0.05)*10)/10); if(quiet) printf(","); if(debug) {
 printf("\r\n"); printf(" Iterations = "); printf("%d\r\n", stepnum); } /* show geodesic results for comparison... */ geodesic(1); if(debug) { printf("\r\n"); } /*_____ The following is an attempt to describe the "uncertainty blob" with another method. Each of the vectors are swung in each plane separately toward the other vector. The resulting inscribed shape is visualized as a distorted wedge. The final step is a computing of the center of mass of this wedge (with a lot of assumptions!). This seems to be a wild goose chase, but I left in here anyhow. -----*/ /* try reducing el to see if converging */ dp = dc = gc;ex = e1;el -= TENTHDEG; geodesic(0); /* if better, this is the upper vector */ if(qc < dp)if(debug) printf("v1 is higher\r\n"); while(gc < dp) { dp = gc; el -= TENTHDEG; gl = ga;

```
geodesic(0);
   } /* now move azimuth to intersect other vector */
   e1 = ex;
   geodesic(0);
   dp = dc = gc;
   ax = a1;
   /* move positive... */
   while( gc <= dp )
   {
      dp = gc;
      al += TENTHDEG;
      g2 = ga;
      geodesic(0);
   }
   /* move negative in case wrong direction */
   dp = dc = gc;
   while( gc <= dp )
   {
      dp = gc;
      al -= TENTHDEG;
      g2 = ga;
      geodesic(0);
   }
   a1 = ax;
   /* now move other azimuth to intersect this vector */
   geodesic(0);
   dp = dc = gc;
   ax = a2i
   /* move negative... */
   while( gc <= dp )
   {
      dp = gc;
      a2 -= TENTHDEG;
      g3 = ga;
      geodesic(0);
   }
   a2 = ax;
   /\,{}^{\star} now move other elevation to intersect this vector {}^{\star}/
   geodesic(0);
   dp = dc = gc;
   ex = e2i
   /* move positive... */
   while( gc <= dp )
   {
      dp = gc;
      e2 += TENTHDEG;
      g4 = ga;
      geodesic(0);
   }
   e^2 = e^i
}
else
{
   /* try other vector */
    dp = dc;
   e1 = ex;
   ex = e2;
   el += TENTHDEG;
   e2 -= TENTHDEG;
   geodesic(0);
   /* if better, this is the upper vector */
   if(gc < dp)
   {
      if(debug)
         printf( "v2 is higher\r\n" );
      while( gc < dp )</pre>
      {
           dp = gc;
         e2 -= TENTHDEG;
         g1 = ga;
         geodesic(0);
      }
      /\,{}^{\star} now move azimuth to intersect other vector \,{}^{\star}/
      e2 = ex;
      geodesic(0);
```

}

if((g1 > gmin) && (g1 < gmax))

```
dp = dc = gc;
      ax = a2;
      /* move positive... */
      while( gc <= dp )</pre>
      ł
         dp = gc;
         a2 += TENTHDEG;
         g2 = ga;
         geodesic(0);
      }
      /* move negative in case wrong direction */
      dp = dc = gc;
      while( gc <= dp )
      {
         dp = gc;
         a2 -= TENTHDEG;
         g2 = ga;
         geodesic(0);
      }
      a2 = ax;
      /* now move other azimuth to intersect this vector */
      geodesic(0);
      dp = dc = gc;
      ax = a1;
      /* move negative... */
      while( gc <= dp )</pre>
      {
         dp = gc;
         al -= TENTHDEG;
         g3 = ga;
         geodesic(0);
      }
      a1 = ax;
      /* now move other elevation to intersect this vector */
      geodesic(0);
      dp = dc = gc;
      ex = e1;
      /* move positive... */
      while( gc <= dp )</pre>
      {
         dp = gc;
         e1 += TENTHDEG;
         g4 = ga;
         geodesic(0);
      }
      e1 = ex;
   }
   élse
   {
      if( debug )
        printf( "v1/v2 are close\r\n" );
      /* can't get better than this */
      gl = ga;
      g2 = ga;
      g3 = ga;
      g4 = ga;
   }
gmin = g1;
if(g2 < gmin)
   gmin = g2;
if(g3 < gmin)
  gmin = g3;
if(g4 < gmin)
   gmin = g4;
gmax = g1;
if (g2 > gmax)
   gmax = g2;
if(g3 > gmax)
  gmax = g3;
if(g4 > gmax)
   gmax = g4;
```

```
{
     ga = g1;
  else if( (g2 > gmin) && (g2 < gmax) )
   ł
     ga = g2;
   else if( (g3 > gmin) && (g3 < gmax) )
   {
     ga = g3;
  else if( (g4 > gmin) && (g4 < gmax) )
   ł
     ga = g4;
   }
   if( (gl != ga) && (gl > gmin) && (gl < gmax) )
   {
     gmax = g1;
  else if( (g2 != ga) && (g2 > gmin) && (g2 < gmax) )
     gmax = g2;
  else if( (g3 != ga) && (g3 > gmin) && (g3 < gmax) )
   ł
     gmax = q3;
   else if( (g4 != ga) && (g4 > gmin) && (g4 < gmax) )
   ł
     gmax = g4;
   }
  gmin = ga;
  if (gmin > gmax)
   {
     ga = gmin;
     gmin = gmax;
     gmax = ga;
   }
  gc = fabs(gmax-gmin)/2;
  ga = gmin + gc;
  gc /= ga;
  if( !quiet )
   {
     printf( "\r\n" );
   }
  if( debug )
     printf("Blob coords: %g, %g, %g, %g\r\n", g1, g2, g3, g4 );
  if( !quiet )
   {
     printf("Blob method = " );
   }
  else
   {
     printf(", ");
   }
  printf( "%g, %g%%\r\n", floor((ga+0.05)*10)/10, floor((gc*100+0.05)*10)/10 );
  return( 0 );
}
/*_____
                               -----
 A standard Geodesic computation, used for comparison.
                                                       _____* /
void geodesic( int pr )
ł
  double f,d1,d2;
  f = \sin(e1)*\sin(e2) - \cos(e1)*\cos(e2)*(\cos(a1)*\cos(a2)-\sin(a1)*\sin(a2));
  d1 = bl*(cos(e1)*cos(a1)+f*cos(e2)*cos(a2))/(1-f*f);
```

```
d2 = bl*(cos(e2)*cos(a2)+f*cos(e1)*cos(a1))/(1-f*f);
```

```
ga = dl*d2*(sin(el)+sin(e2))/(dl+d2);
gc = bl*fabs( (cos(e2)*sin(el)*sin(a2)-cos(el)*sin(e2)*sin(al))/(ga*sqrt(1-f*f)) );
if( pr )
{
    if(!quiet)
    {
        printf( "\r\n" );
        printf( " Geodesic =" );
    }
    printf( " %g, %g%%", floor((ga+0.05)*10)/10, floor(((gc*100)+0.05)*10)/10 );
}
```

APPENDIX B: CONVERGENCE TEST DATA

1) Low Elevation Both near baseline One moving up in elevation

2) Low Elevation One near baseline Other moving away from baseline

3) Low Elevation Both start 1/3 from baseline One moving away from baseline

4) Low Elevation Both start 1/3 from baseline One moving up in elevation

5) Low Elevation Both start 2/3 from baseline One moving up in elevation

6) Low Elevation Both start 2/3 from baseline One moving away from baseline

7) Medium Elevation Both start near from baseline One moving away from baseline

8) High Elevation Both start near from baseline One moving away from baseline

9) High Elevation Both start 1/3 from baseline One moving away from baseline

10) High Elevation Both start 2/3 from baseline One moving up in eleavation

11) Low Elevation One 120deg from baseline One moving up in eleavation

Low Elevation Both near baseline One moving up in elevation

BL	A1	E1	A2	E2	GEO		HIT	
100 100	10 10	20 20	10 10	20 21	18.5, 19 0.	0%, 2.2%,	18.5, 19 1.	0.2%, 1.2%,
100	10	20	10	22	19.5,	4.3%,	19.6,	2.4%,
100	10	20	10	23	19.9,	6.2%,	20.1,	3.4%,
100	10	20	10	24	20.4,	8.0%,	20.6,	4.3%,
100	10	20	10	25	20.8,	9.6%,	21.1,	5.1%,
100	10	20	10	26	21.3,	11.2%,	21.6,	5.9%,
100	10	20	10	27	21.7,	12.6%,	22.1,	6.7%,
100	10	20	10	28	22.1,	13.9%,	22.5,	7.3%,
100	10	20	10	29	22.5,	15.2%,	22.9,	8.0%,
100	10	20	10	30	22.9,	16.4%,	23.3,	8.6%,
100	10	20	10	31	23.3,	17.5%,	23.7,	9.1%,
100	10	20	10	32	23.6,	18.6%,	24.1,	9.6%,
100	10	20	10	33	24.0,	19.6%,	24.5,	10.1%,
100	10	20	10	34	24.3,	20.5%,	24.8,	10.6%,
100	10	20	10	35	24.7,	21.4%,	25.2,	11.0%,
100	10	20	10	36	25.0,	22.3%,	25.5,	11.5%,
100	10	20	10	37	25.3,	23.1%,	25.9,	11.9%,
100	10	20	10	38	25.7,	23.9%,	26.2,	12.2%,
100	10	20	10	39	26.0,	24.7%,	26.5,	12.6%,
100	10	20	10	40	26.3,	25.4%,	26.8,	12.9%,

Low Elevation One near baseline Other moving away from baseline

BL	A1	E1	A2	E2	GEO		HIT	
100	10	20	10	20	18.5,	0%,	18.5,	0.2%,
100	10	20	11	20	18.5,	4.2%,	18.7,	2.3%,
100	10	20	12	20	18.5,	8.3%,	18.8,	4.6%,
100	10	20	13	20	18.5,	12.4%,	19.0,	6.9%,
100	10	20	14	20	18.6,	16.3%,	19.2,	9.1%,
100	10	20	15	20	18.6,	20.2%,	19.4,	11.3%,
100	10	20	16	20	18.6,	24.0%,	19.5,	13.4%,
100	10	20	17	20	18.6,	27.7%,	19.7,	15.5%,
100	10	20	18	20	18.6,	31.3%,	19.9,	17.5%,
100	10	20	19	20	18.6,	34.8%,	20.1,	19.5%,
100	10	20	20	20	18.5,	38.3%,	20.3,	21.5%,
100	10	20	21	20	18.5,	41.7%,	20.4,	23.5%,
100	10	20	22	20	18.5,	45.1%,	20.6,	25.4%,
100	10	20	23	20	18.5,	48.4%,	20.8,	27.2%,
100	10	20	24	20	18.4,	51.6%,	21.0,	29.1%,
100	10	20	25	20	18.4,	54.8%,	21.1,	30.9%,
100	10	20	26	20	18.3,	57.9%,	21.3,	32.6%,
100	10	20	27	20	18.3,	61.0%,	21.5,	34.4%,
100	10	20	28	20	18.2,	64.0%,	21.7,	36.1%,
100	10	20	29	20	18.2,	67.0%,	21.9,	37.8%,
100	10	20	30	20	18.1,	70.0%,	22.0,	39.4%,

Low Elevation Both start 1/3 from baseline One moving away from baseline BL A1 E1 A2 E2 GEO HIT_____ 21.0, 0%, 21.0, 0.1%, 100 30 20 30 20

 21.0,
 0%,

 21.1,
 2.4%,

 21.2,
 4.7%,

 21.3,
 7.0%,

 21.4,
 9.2%,

 21.5,
 11.4%,

 21.3, 2.1%, 100 30 20 31 20 21.5, 4.1%, 100 30 20 32 20 21.8, 6.0%, 100 30 20 33 20 22.0, 100 30 20 34 20 7.9%, 22.0, 7.9%, 22.3, 9.8%, 22.6, 11.6%, 100 30 20 35 20 21.6, 13.5%, 100 30 20 36 20 100 30 20 37 20 21.7, 15.5%, 22.8, 13.4%, 21.8, 17.5%, 100 30 20 38 20 23.1, 15.1%, 21.9, 19.4%, 23.3, 16.8%, 100 30 20 39 20 22.0, 21.3%, 100 30 20 40 20 23.6, 18.5%, 22.0, 23.1%, 23.9, 20.1%, 100 30 20 41 20 24.2, 21.6%, 100 30 20 42 20 22.1, 24.9%, 24.4, 23.2%, 100 30 20 43 20 22.2, 26.6%, 22.3, 28.3%, 24.7, 24.7%, 100 30 20 44 20 22.4, 29.9%, 25.0, 26.1%, 100 30 20 45 20 22.5, 31.5%, 25.2, 27.6%, 100 30 20 46 20 100 30 20 47 20 22.5, 33.1%, 25.5, 29.0%, 25.8, 30.3%, 22.6, 34.6%, 100 30 20 48 20 22.7, 36.1%, 26.1, 31.6%, 100 30 20 49 20 22.8, 37.5%, 26.4, 32.9%, 100 30 20 50 20

Low Elevation Both start 1/3 from baseline One moving up in elevation

BL	A1	E1	A2	E2	GEO		HIT	
100	30	20	30	20	21.0,	0%,	21.0,	0.1%,
100	30	20	30	21	21.6,	4.3%,	21.8,	3.5%,
100	30	20	30	22	22.1,	8.3%,	22.6,	6.7%,
100	30	20	30	23	22.7,	12.1%,	23.3,	9.5%,
100	30	20	30	24	23.3,	15.7%,	24.0,	12.0%,
100	30	20	30	25	23.8,	19.1%,	24.7,	14.4%,
100	30	20	30	26	24.4,	22.3%,	25.3,	16.5%,
100	30	20	30	27	24.9,	25.3%,	25.9,	18.5%,
100	30	20	30	28	25.5,	28.3%,	26.5,	20.3%,
100	30	20	30	29	26.0,	31.0%,	27.0,	22.0%,
100	30	20	30	30	26.5,	33.7%,	27.6,	23.6%,
100	30	20	30	31	27.0,	36.2%,	28.0,	25.0%,
100	30	20	30	32	27.6,	38.7%,	28.5,	26.4%,
100	30	20	30	33	28.1,	41.0%,	29.0,	27.7%,
100	30	20	30	34	28.5,	43.2%,	29.4,	28.9%,
100	30	20	30	35	29.0,	45.4%,	29.8,	30.1%,
100	30	20	30	36	29.5,	47.5%,	30.2,	31.2%,
100	30	20	30	37	30.0,	49.5%,	30.6,	32.3%,
100	30	20	30	38	30.4,	51.4%,	31.0,	33.3%,
100	30	20	30	39	30.9,	53.3%,	31.3,	34.2%,
100	30	20	30	40	31.3,	55.1%,	31.6,	35.1%,

Low Elevation Both start 2/3 from baseline One moving up in elevation

BL	A1	E1	A2	E2	GEO		HIT	
100	60	20	60	20	36.4,	0%,	36.4,	0.1%,
100	60	20	60	21	37.4,	4.9%,	38.1,	6.0%,
100	60	20	60	22	38.3,	9.5%,	39.5,	11.4%,
100	60	20	60	23	39.3,	14.0%,	40.8,	16.2%,
100	60	20	60	24	40.2,	18.3%,	41.8,	20.5%,
100	60	20	60	25	41.1,	22.4%,	42.6,	24.5%,
100	60	20	60	26	41.9,	26.3%,	43.3,	28.2%,
100	60	20	60	27	42.7,	30.1%,	43.9,	31.6%,
100	60	20	60	28	43.5,	33.8%,	44.3,	34.8%,
100	60	20	60	29	44.3,	37.4%,	44.7,	37.8%,
100	60	20	60	30	45.0,	40.9%,	44.9,	40.7%,
100	60	20	60	31	45.7,	44.3%,	45.0,	43.4%,
100	60	20	60	32	46.4,	47.7%,	45.1,	46.1%,
100	60	20	60	33	47.0,	50.9%,	45.1,	48.6%,
100	60	20	60	34	47.5,	54.2%,	45.1,	51.0%,
100	60	20	60	35	48.0,	57.3%,	45.0,	53.3%,
100	60	20	60	36	48.5,	60.5%,	44.9,	55.6%,
100	60	20	60	37	48.9,	63.6%,	44.8,	57.7%,
100	60	20	60	38	49.3,	66.7%,	44.6,	59.9%,
100	60	20	60	39	49.6,	69.7%,	44.4,	61.9%,
100	60	20	60	40	49.9,	72.8%,	44.2,	63.9%,

Low Elevation Both start 2/3 from baseline One moving away from baseline

BL	A1	E1	A2	E2	GEO		HIT	
100	60	20	60	20	36.4,	0%,	36.4,	0.1%,
100	60	20	61	20	37.0,	0.9%,	37.1,	1.2%,
100	60	20	62	20	37.5,	1.8%,	37.8,	2.3%,
100	60	20	63	20	38.1,	2.6%,	38.6,	3.4%,
100	60	20	64	20	38.7,	3.4%,	39.3,	4.4%,
100	60	20	65	20	39.4,	4.2%,	40.1,	5.4%,
100	60	20	66	20	40.0,	4.9%,	40.9,	6.4%,
100	60	20	67	20	40.7,	5.7%,	41.8,	7.3%,
100	60	20	68	20	41.4,	6.3%,	42.6,	8.2%,
100	60	20	69	20	42.1,	7.0%,	43.5,	9.0%,
100	60	20	70	20	42.8,	7.6%,	44.4,	9.8%,
100	60	20	71	20	43.6,	8.2%,	45.3,	10.6%,
100	60	20	72	20	44.4,	8.7%,	46.3,	11.3%,
100	60	20	73	20	45.3,	9.2%,	47.3,	12.0%,
100	60	20	74	20	46.1,	9.7%,	48.3,	12.6%,
100	60	20	75	20	47.0,	10.2%,	49.4,	13.2%,
100	60	20	76	20	48.0,	10.6%,	50.5,	13.8%,
100	60	20	77	20	49.0,	11.0%,	51.6,	14.3%,
100	60	20	78	20	50.0,	11.4%,	52.8,	14.8%,
100	60	20	79	20	51.1,	11.7%,	54.1,	15.3%,
100	60	20	80	20	52.2,	12.0%,	55.4,	15.7%,

Medium Elevation Both start near from baseline One moving away from baseline BL A1 E1 A2 E2 GEO HIT_____ 100 20 45 20 45 53.2, 0%, 53.2, 0%, 53.4, 1.5%, 53.5, 0.8%, 100 20 45 21 45

 53.4,
 1.5%,

 53.5,
 3.1%,

 53.7,
 4.6%,

 53.9,
 6.1%,

 53.9, 100 20 45 22 45 1.6%, 54.2, 2.4%, 100 20 45 23 45 100 20 45 24 45 54.5, 3.2%, 54.1, 7.5%, 54.2, 9.0%, 100 20 45 25 45 54.8, 4.0%, 100 20 45 26 45 4.7%, 55.1, 54.4, 10.4%, 100 20 45 27 45 55.5, 5.5%, 100 20 45 28 45 54.6, 11.8%, 55.8, 6.3%, 100 20 45 29 45 54.7, 13.2%, 56.1, 7.0%, 56.4, 100 20 45 30 45 54.9, 14.6%, 7.7%, 56.8, 55.1, 16.0%, 100 20 45 31 45 8.4%, 55.3, 17.3%, 100 20 45 32 45 57.1, 9.2%, 57.4, 9.9%, 100 20 45 33 45 55.4, 18.7%, 57.8, 10.5%, 100 20 45 34 45 55.6, 20.0%, 100 20 45 35 45 55.8, 21.2%, 58.1, 11.2%, 55.9, 22.5%, 58.4, 11.9%, 100 20 45 36 45 100 20 45 37 45 56.1, 23.8%, 58.8, 12.6%, 100 20 45 38 45 56.3, 25.0%, 59.1, 13.2%, 56.5, 26.2%,59.5, 13.9%,56.6, 27.4%,59.8, 14.5%, 100 20 45 39 45 100 20 45 40 45

High Both One	n El n st mov	leva cart ving	atio z ne g av	on ear way	from base from base	line line		
BL	A1	E1	A2	E2	GEO		HIT	
100	20	70	20	70	146.2,	0%,	146.2,	0%,
100	20	70	21	70	146.7,	0.6%,	146.8,	0.3%,
100	20	70	22	70	147.1,	1.2%,	147.4,	0.6%,
100	20	70	23	70	147.6,	1.8%,	148.0,	0.9%,
100	20	70	24	70	148.1,	2.3%,	148.7,	1.2%,
100	20	70	25	70	148.6,	2.9%,	149.3,	1.5%,
100	20	70	26	70	149.0,	3.5%,	149.9,	1.7%,
100	20	70	27	70	149.5,	4.0%,	150.6,	2.0%,
100	20	70	28	70	150.0,	4.6%,	151.2,	2.3%,
100	20	70	29	70	150.5,	5.2%,	151.8,	2.6%,
100	20	70	30	70	151.0,	5.7%,	152.5,	2.9%,
100	20	70	31	70	151.5,	6.3%,	153.1,	3.1%,
100	20	70	32	70	152.0,	6.8%,	153.8,	3.4%,
100	20	70	33	70	152.5,	7.3%,	154.4,	3.7%,
100	20	70	34	70	153.0,	7.9%,	155.1,	3.9%,
100	20	70	35	70	153.5,	8.4%,	155.8,	4.2%,
100	20	70	36	70	154.1,	8.9%,	156.4,	4.4%,
100	20	70	37	70	154.6,	9.4%,	157.1,	4.7%,
100	20	70	38	70	155.1,	9.9%,	157.8,	5.0%,
100	20	70	39	70	155.7,	10.4%,	158.5,	5.2%,
100	20	70	40	70	156.2,	10.9%,	159.2,	5.5%,

High Elevation Both start 1/3 from baseline One moving away from baseline

BL	A1	E1	A2	E2	GEO		HIT	
100	30	70	30	70	158.6,	0%,	158.6,	0%,
100	30	.70	31	.70	159.4,	0.5%,	159.6,	0.3%,
100	30	70	32	70	160.2,	1.1%,	160.5,	0.5%,
100	30	70	33	70	161.1,	1.6%,	161.5,	0.8%,
100	30	70	34	70	161.9,	2.1%,	162.5,	1.1%,
100	30	70	35	70	162.7,	2.6%,	163.5,	1.3%,
100	30	70	36	70	163.6,	3.1%,	164.5,	1.6%,
100	30	70	37	70	164.4,	3.6%,	165.5,	1.8%,
100	30	70	38	70	165.3,	4.1%,	166.5,	2.1%,
100	30	70	39	70	166.2,	4.6%,	167.5,	2.3%,
100	30	70	40	70	167.1,	5.1%,	168.6,	2.6%,
100	30	70	41	70	168.0,	5.6%,	169.6,	2.8%,
100	30	70	42	70	168.9,	6.1%,	170.7,	3.1%,
100	30	70	43	70	169.8,	6.5%,	171.7,	3.3%,
100	30	70	44	70	170.7,	7.0%,	172.8,	3.5%,
100	30	70	45	70	171.7,	7.4%,	173.9,	3.8%,
100	30	70	46	70	172.6,	7.9%,	175.0,	4.0%,
100	30	70	47	70	173.6,	8.3%,	176.1,	4.2%,
100	30	70	48	70	174.6,	8.7%,	177.2,	4.4%,
100	30	70	49	70	175.6,	9.2%,	178.4,	4.6%,
100	30	70	50	70	176.6,	9.6%,	179.6,	4.8%,

High Elevation Both start 2/3 from baseline One moving up in eleavation

BL	A1	E1	A2	E2	GEO		HIT	
100	60	70	60	70	274.7,	0%,	274.8,	0%,
100	60	70	60	71	281.8,	1.6%,	282.5,	0.8%,
100	60	70	60	72	287.9,	3.3%,	289.2,	1.7%,
100	60	70	60	73	292.7,	4.9%,	294.6,	2.5%,
100	60	70	60	74	296.1,	6.6%,	298.3,	3.4%,
100	60	70	60	75	297.8,	8.3%,	300.3,	4.2%,
100	60	70	60	76	297.6,	10.1%,	300.4,	5.1%,
100	60	70	60	77	295.4,	11.9%,	298.5,	6.1%,
100	60	70	60	78	291.1,	13.9%,	294.5,	7.0%,
100	60	70	60	79	284.7,	16.1%,	288.5,	8.1%,
100	60	70	60	80	276.3,	18.4%,	280.6,	9.2%,
100	60	70	60	81	266.1,	20.9%,	271.0,	10.4%,
100	60	70	60	82	254.3,	23.7%,	259.9,	11.7%,
100	60	70	60	83	241.1,	26.8%,	247.7,	13.1%,
100	60	70	60	84	226.9,	30.3%,	234.5,	14.7%,
100	60	70	60	85	212.0,	34.2%,	220.8,	16.5%,
100	60	70	60	86	196.7,	38.6%,	206.8,	18.4%,
100	60	70	60	87	181.4,	43.6%,	192.7,	20.5%,
100	60	70	60	88	166.3,	49.2%,	, 178.8	22.9%,
100	60	70	60	89	151.5,	55.7%,	165.2,	25.5%
100	60	70	60	90	137.4,	63.0%,	152.1,	28.5%,

NAR 52094, August 1996

Hemispherical Iteration Tracking Method Convergence Test 11

Low Elevation One 120deg from baseline One moving up in eleavation

BL	Al I	31 Z	42 E	E2	GEO		HIT		BLOB	
100 100	120 120	30 30	30 30	10 11	37.0, 39.4,	55.5%, 46.8%,	27.6, 30.4,	56.8%, 47.0%,	28.4, 7.4% 30.6, 10.1%	
100	120	30	30	12	41.7,	38.8%,	33.5,	38.3%,	32.7, 12.5%	
100	120	30	30	13	44.2,	31.5%,	36.7,	30.6%,	35.6, 12.2%	
100	120	30	30	14	46.7,	24.8%,	40.2,	23.7%,	39.1, 10.4%	
100	120	30	30	15	49.2,	18.5%,	43.9,	17.4%,	42.8, 8.4%	
100	120	30	30	16	51.7,	12.7%,	47.8,	11.8%,	46.7, 6.2%	
100	120	30	30	17	54.2,	7.2%,	51.8,	6.6%,	51.0, 3.9%	
100	120	30	30	18	56.7,	2.1%,	55.9,	1.9%,	55.6, 1.2%	
100	120	30	30	19	59.1,	2.7%,	61.1,	2.4%,	59.4, 0.4%	
100	120	30	30	20	61.5,	7.3%,	67.0,	6.2%,	62.3, 1.2%	
100	120	30	30	21	63.8,	11.6%,	72.9,	9.6%,	65.1, 2.1%	
100	120	30	30	22	66.0,	15.9%,	78.5,	12.8%,	68.0, 2.9%	
100	120	30	30	23	68.0,	19.9%,	83.7,	15.8%,	70.8, 3.9%	
100	120	30	30	24	69.9,	23.9%,	88.2,	18.7%,	73.5, 4.9%	
100	120	30	30	25	71.5,	27.8%,	91.8,	21.6%,	76.2, 6.1%	
100	120	30	30	26	73.0,	31.7%,	94.3,	24.6%,	78.7, 7.3%	
100	120	30	30	27	74.1,	35.7%,	95.4,	27.7%,	81.2, 8.7%	
100	120	30	30	28	75.0,	39.6%,	95.3,	31.0%,	83.6, 10.2%	
100	120	30	30	29	75.6,	43.7%,	93.7,	34.8%,	85.8, 11.9%	
100	120	30	30	30	75.8,	47.9%,	90.9,	38.9%,	87.9, 13.7%	

SUMMARY

Historically, the choice of formulae for model rocketry altitude data reduction has been limited to linear closed-form equations. Using simple trigonometric functions, these equations require only a pocket calculator or, if necessary, could be derived by hand using sine and cosine tables. In recent years the widespread availability of programmable calculators and portable computers has automated these calculations. In fact, the typical portable computer has more than enough computing power to perform vastly more complex methods of data reduction beyond the static closed-form algorithms.

The main objective of this project was to implement a computer software program for a more accurate method of determining a model rocket's likely altitude given twostation theodolite angles. The mathematical basis of the new method has a strong similarity to the closed form Geodesic method, but adds weighting for real-world effects of optically tracking a model rocket to ejection. The grouping of errors into a "region of uncertainty" is approximated by a hemispherical shape which is located using an iterative software technique, hence the name "Hemispherical Iteration Tracking".

The software was tested for various regions in 3D space relative to the trackers and the convergence of the HIT method was compared to the Geodesic method with favorable results. Additionally, a set of data from a particularly problematic NAR-sanctioned regional was used to compare the new method with the Geodesic equations; the results showed that the closure rate would have improved from only 31% of tracked flights closed to over 88% closed.

NAR competitors would benefit from this new data reduction method by improving the closure rate for altitude events, offering a more even playing field when existing algorithms fail to close reliably under certain conditions. Further statistical analysis would be needed before approving the new method for NAR-sanctioned competition and record attempts.

(297 words)